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Draft Indian Standard

BRIX HYDROMETERS – SPECIFICATION
(*Second Revision*)

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ICS 17.060

Glass, Glassware & Laboratoryware Sectional Committee, CHD 10

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FOREWORD

(Formal Clauses to be added later)

This standard was first published in 1974 for Brix hydrometers which are mainly used by the sugar industry for determining the percentage of total dissolved solid content. However, keeping in view that most of the sugar units were in the practice of using these hydrometers with built-in thermometers and also that International Organization for Standardization (ISO), has published documents on this item, the Sectional Committee responsible for the preparation of this standard, revised it in 1986 in order to help the manufacturers to produce Brix thermo-hydrometers also for sugar industry in rational shapes and sizes in conformity with this standard.

The second revision of this standard is undertaken in view of the technological advancements taken place in the industry. Several editorial changes such as inclusion of ICS No., Hindi Title, Reference Clause, and statutory changes such as the BIS Certification Marking clause as per the BIS Act 2016 have also been incorporated.

Brix hydrometers and thermo-hydrometers prescribed in this standard are based on L50 series of density hydrometers [*see* **IS 3104 (Part 1) : 1982** and **IS 3104 (Part 2) : 1982**].

In the formulation of this standard due weightage has been given to the available data relating to tables for conversion of degree Brix to relative density ($20^{\circ}/4^{\circ}\text{C}$) and corrections on account of thermal expansions of glass, liquid solutions, etc.

For the purpose of deciding whether a particular requirement of this standard is complied with, the final value, observed or calculated, expressing the result of a test or analysis, shall be rounded off in accordance with IS 2 : 2022 'Rules for rounding off numerical values (second revision)'. The number of significant places retained in the rounded off value should be the same as that of the specified value in this standard.

BRIX HYDROMETERS – SPECIFICATION (*Second Revision*)

1 SCOPE

This standard prescribes requirements and methods of sampling and test for Brix hydrometers and Brix thermo-hydrometers meant for use in sugar industry for determining the percentage by mass of sucrose in a pure sucrose solution at 20°C.

2 REFERENCE

The standards listed below contain provisions which through reference in this text, constitute provisions of and necessary adjuncts to this standard. At the time of publication, the editions indicated were valid. All standards are subject to revision and parties to agreements based on this standard are encouraged to investigate the possibility of applying the most recent editions of the standards indicated.

| <i>IS No.</i> | <i>IS Titles</i> |
|------------------------|--|
| 1382 : 1981 | Glossary of terms relating to glass and glassware (<i>first revision</i>) |
| 8787 : 2018 | Principles of design, construction and use of liquid-in-glass thermometers (<i>first revision</i>) |
| 6274 : 1971 | Method of calibrating liquid-in-glass thermometers |
| 3104 (Part 1) : 1982 | Specification for density hydrometers: Part 1 Requirements (<i>first revision</i>) |
| 5717 : 2003 | Laboratory glassware - Pyknometers (<i>second revision</i>) |
| 4825 : 1982 | Specification for liquid - In - Glass solid - Stem reference thermometers (<i>first revision</i>) |
| 9621 : 1980 | Principles of construction and adjustment of glass hydrometers |

3 TERMINOLOGY

3.1 For the purpose of this standard, the definitions given in IS 1382 in addition to those given below, shall apply.

3.2 Bulb — The wider portion of a hydrometer containing the loading material.

3.3 Stem — The thin tubing attached to the upper part of the bulb containing the indicating scale.

3.4 Degree Brix — The percentage by mass of sucrose in a pure sucrose solution at 20°C.

4 TEMPERATURE OF CALIBRATION AND RANGE OF SCALES

4.1 Temperature of Calibration — The hydrometers and thermo-hydrometers shall be calibrated at 20°C.

4.2 Range of Scales — The hydrometers and thermo-hydrometers in a set shall cover the entire range from 0 to 100° Brix in steps of 10 degrees each hydrometer.

5 SURFACE TENSION

5.1 Brix hydrometers and thermo-hydrometers shall be graduated on the basis of 'high' surface tension category, that is, 75 mN/m.

6 REFERENCE MARK

6.1 A reference mark consisting of a short horizontal straight line with a 'V' at each end (like) shall be marked on the paper scale a few millimetres above the topmost graduation mark.

6.2 A fine, clear and permanent line of uniform thickness shall be etched on the stem of the hydrometer coincident with the horizontal portions of the reference mark, but slightly longer than the reference mark, so that the ends of the etched line project into the 'V' at either ends of the reference mark. This arrangement ensures that any displacement of the paper scale is readily apparent.

6.2.1 Similarly, a suitable datum line shall be marked for thermometer scale also in thermo-hydrometers.

7 DESIGNATION

7.1 Brix hydrometers and thermo-hydrometers shall be designated by the letter 'B' and the minimum value of the range of scale separated by an oblique stroke. For example, a Brix hydrometer or thermo-hydrometer having a range from 10 to 20° Brix shall be designated as B/10.

8 REQUIREMENTS

8.1 The brix hydrometers and brix thermo-hydrometers shall conform to the design requirements given in IS 9621.

8.2 Materials

8.2.1 *Glass*

The bulb and stem of hydrometers and thermo-hydrometers shall be made of colourless transparent glass, resistant to chemicals and thermal shock encountered in use. It shall be as free as possible from strain and visual defects.

8.2.1.1 The recommended coefficient of cubical thermal expansion of glass used in the manufacture of Brix hydrometers is 25.0×10^{-6} per degree Celsius.

NOTE — The conventional value for the coefficient of cubical thermal expansion of glass used in the manufacture of hydrometers is 25×10^{-6} per °C. In case of a significant departure from this value, the actual coefficient shall be indicated on the hydrometers and thermo-hydrometers so that appropriate correction may be applied to the readings by making reference to Table 4 (*see B-4.3.1*).

8.2.2 *Loading Material*

8.2.2.1 The loading material shall be confined to the bottom of the bulb. After the instrument has been maintained in a horizontal position for 1 hour at 80°C and subsequently cooled in that position, it shall meet the requirement of **8.3**.

NOTE — The use of mercury as a loading material is not permitted.

8.2.2.2 There shall be no loose material whatsoever in any other part of the instrument.

8.3 Pattern, Workmanship and Finish

8.3.1 The hydrometers and thermo-hydrometers shall be of a pattern as shown in Fig. 1A and 1B. They shall be circular in cross section, robust and symmetrical around the main axis. They shall float vertically in sucrose solutions of appropriate density at 20°C corresponding to their lowest graduation and the inclination, if any, from the vertical shall not exceed 1.5°.

8.3.2 In thermo-hydrometers, the thermometer scale shall conform to the design requirements given in IS 8787 and those given in Table 1.

TABLE 1 Requirements for Thermometer for a Brix Thermo-Hydrometer
(Clause 8.3.2)

| SL No. | CHARACTERISTIC | REQUIREMENT |
|-----------|--|---------------|
| (1) | (2) | (3) |
| i) | Range of thermometer | 0° to 40°C |
| ii) | Immersion | Total |
| iii) | Subdivision | 0.5°C |
| iv) | Scale error at any point | ± 0.5°C |
| v) | Scale length (<i>Min</i>) | 64 mm |
| vi) | Extension of scale on either side | 4 graduations |
| vii) | Expansion chamber to withstand temperature rise up to (<i>Min</i>) | 85°C |

NOTE — The bulb of the thermometer should form an integral part of hydrometer.

8.4 Scales

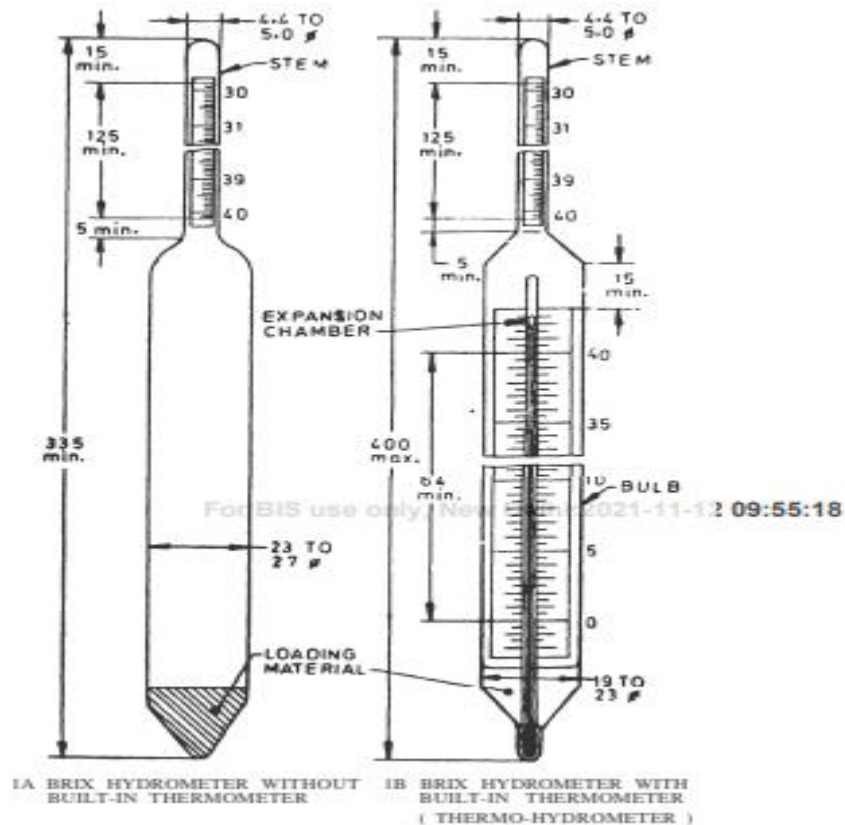
8.4.1 The scales and the inscriptions shall be marked on a smooth matt surface of white or off-white colour. It shall be straight and free from twist. Neither the scales nor the graduations shall distort or discolour when the instrument is maintained at a temperature of 80°C for 24 hours. The hydrometer scale shall be fully enclosed in the hydrometer with all graduation marks clearly visible on the stem.

8.4.2 The graduation lines shall be distinct and of uniform thickness not exceeding 0.2 mm. There shall be no evident local irregularities in their spacing. They shall be perpendicular to the axis of the hydrometer.

8.4.3 The graduations of thermometers when provided shall be in accordance to **9.1** of IS 8787.

8.4.4 The highest and the lowest graduation lines indicating the nominal range of the hydrometer shall be long lines and the distance between them shall be divided into 100 equal parts. Thus the value of the scale interval shall be 0.1° Brix.

8.4.4.1 In addition to the above, two to four extra smallest scale divisions shall be marked on either ends of the scale.



All dimensions in millimeters

FIG. 1 BRUX HYDROMETERS

8.4.5 The length of long lines shall be not less than half the circumference of the stem that of medium lines one-third of the circumference, and of short lines one-fifth of the circumference.

8.4.6 *Sequence of Graduation Lines*

8.4.6.1 Every tenth graduation line shall be a long line. There shall be a medium line between two consecutive long lines and four short lines between consecutive medium and long lines.

8.4.6.2 The sequence of graduation lines in thermometers of thermo-hydrometers shall be in accordance to **9.1.1** of IS 878.

8.4.7 *Figuring of Graduation Lines*

8.4.7.1 The highest and the lowest graduation lines referring to the nominal range of the hydrometer and thermohydrometer shall be figured in full. At least every tenth graduation line shall be figured. Graduation lines within the nominal range and the inscription shall be marked in black. Graduation lines outside the nominal range may be marked in colour other than black.

8.4.7.2 The figuring of thermometers, when provided shall be in accordance with **9.1.2** of IS 8787.

8.5 Dimensions

The dimensions of hydrometers shall be as given in Table 2.

Table 2 Dimensions for Brix Hydrometers
 (Clause 8.5)

| SL NO. | DIMENSIONS | VALUES | |
|--------|-----------------------------|------------|-------------------|
| | | Hydrometer | Thermo-hydrometer |
| (1) | (2) | (3) | (4) |
| i) | Overall length, <i>Max</i> | 325 | 400 |
| ii) | Length of scale, <i>Min</i> | 125 | 125 |
| iii) | Diameter of the bulb: | | |
| | <i>Min</i> | 23 | 19 |
| | <i>Max</i> | 27 | 23 |
| iv) | Diameter of the stem: | | |
| | <i>Min</i> | 4.4 | 4.4 |
| | <i>Max</i> | 5.0 | 5.0 |

8.5.1 The cross section of the stem shall remain unchanged for at least 5 mm below the lowest graduation line.

8.5.2 The stem shall extend at least 15 mm above the uppermost graduation line on the scale.

8.5.3 The volume of the bulb below the lowest graduation line shall be between 50 and 65 cm³.

8.5.4 Recommended stem diameters for the ten ranges of the hydrometers are given in Table 3 for the guidance of manufacturers. These stem diameters are suitable for a volume (below the lowest graduation mark) of 58 cm³ and provide for a scale length of about 150 mm.

Table 3 Recommended Stem Diameters for Brix Hydrometers
 (Clause 8.5.4)

| SL NO. | RANGE OF HYDROMETERS SCALE | STEM DIAMETER |
|--------|----------------------------|---------------|
| (1) | (2) | (3) |
| | BRIX | mm |
| i) | 0 to 10 | 4.4 |
| ii) | 10 to 20 | 4.5 |
| iii) | 20 to 30 | 4.6 |
| iv) | 30 to 40 | 4.6 |
| v) | 40 to 50 | 4.7 |
| vi) | 50 to 60 | 4.8 |
| vii) | 60 to 70 | 4.8 |

| | | |
|-------|-----------|-----|
| viii) | 70 to 80 | 4.9 |
| ix) | 80 to 90 | 4.9 |
| x) | 90 to 100 | 4.9 |

8.6 Accuracy

8.6.1 The error at any point on the scale of the hydrometer shall not exceed $\pm 0.1^\circ$ Brix.

8.6.1.1 The accuracy of the hydrometers shall be tested in accordance with the method prescribed in **Annex A**.

8.6.2 The accuracy of the thermometer scale shall be tested in accordance with the method prescribed in IS 6274.

9 MARKING AND PACKING

9.1 Marking

Brix hydrometers shall be marked legibly and indelibly with the following information:

- a) Maker's name or recognized trade-mark, if any;
- b) Calibration temperature, that is, '20°C';
- c) Reference mark; and
- d) Designation.

9.2 BIS Certification Marking

The product(s) conforming to the requirements of this standard may be certified as per the conformity assessment schemes under the provisions of the *Bureau of Indian Standards Act, 2016* and the Rules and Regulations framed thereunder, and the products may be marked with the Standard Mark.

9.3 Packing

Brix hydrometers or thermo-hydrometers shall be packed as agreed to between the purchaser and the supplier.

10 SAMPLING

10.1 Representative samples shall be drawn and adjudged for conformity to this standard as prescribed in IS 3104 (Part 1).

11 METHOD OF USING BRIX HYDROMETER

11.1 The methods of applying corrections and determining percentage of sucrose in a solution are given in **Annex B**.

ANNEX A

(Clause 8.6.1.1)

METHOD OF TESTING ACCURACY OF BRIX HYDROMETERS

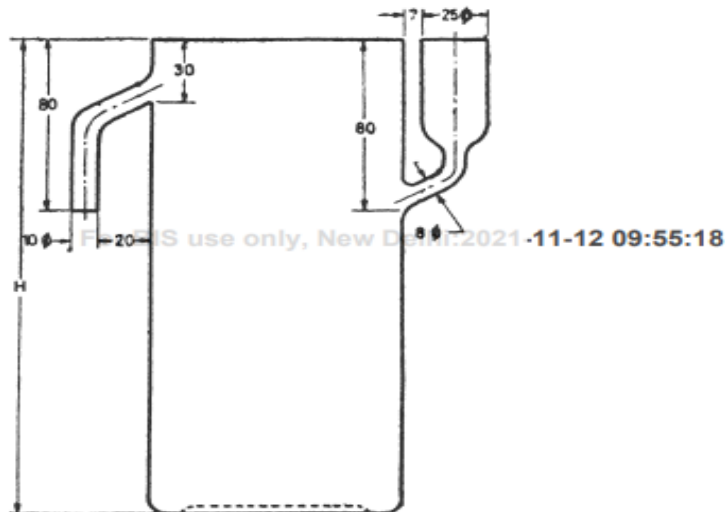
A-1 GENERAL

A-1.1 Accuracy of Brix hydrometers shall be tested by comparison against a similar standardized hydrometer for routine purpose. However, in the case of a dispute this shall be done by verifying the readings of the Brix hydrometer or thermo-hydrometer by determining relative density ($20^{\circ}/4^{\circ}\text{C}$) of a liquid with the help of a pycnometer (*see* **IS 5717**) at appropriate temperature, and converting the value so obtained into degrees Brix.

A-1.2 In the case of testing by comparison, sucrose solution of known concentration shall be used. Alternatively, mixtures of organic liquids like xylene and tetrachloroethylene which have low surface tension (of the order of 35 mN/m) may be used with advantage to avoid surface contamination and removal of surface film periodically. In that case suitable correction shall be applied to the readings of each instrument (*see* **A-4.1.2**).

A-2 APPARATUS

A-2.1 A vessel provided with an arrangement for overflowing of liquid in such a way that the surface film is constantly removed shall be used for taking readings of hydrometers. A recommended type of overflow vessel is shown in Fig. 2.



$$L = 135 \pm 5, W = 55 \pm 3 \text{ and } H = 430 \pm 5$$

All dimensions in millimetres.
FIG. 2 OVERFLOW VESSEL

A-2.2 Thermometer — Solid-stem liquid-in-glass type, of a suitable range and capable of reading with an accuracy of ± 0.1 degree Celsius (*see* **IS 4825**).

A-2.3 Pycnometer — 25 ml capacity of Type 4 (*see* **IS 5717**).

A-2.4 Water-Bath — capable of maintaining a temperature of 20°C.

A-3 LIQUIDS

A-3.1 Sucrose Solution — in water, made to cover at least four points on the scale of the hydrometer.

A-3.2 Xylene

A-3.3 Tetrachloroethylene

A-4 PROCEDURE

A-4.1 Comparison Method

A-4.1.1 Method Using Sucrose Solution — Pour the sucrose solution into the overflow vessel almost to the brim. Stir well to drive out any air bubbles that might be present in it and fill the vessel up to the brim. Insert the standardized Brix hydrometer along with that under test into the solution and allow them to attain the temperature of the liquid. Note the readings of the two hydrometers.

A-4.1.1.1 Any difference in the reading of the Brix hydrometer under test from that of the standardized hydrometer shall be treated as error at that point (*see* **B-4.2**). Repeat the test to cover at least four points on the scale.

A-4.1.2 Method Using Xylene and Tetrachloroethylene — Follow the procedure described in **A-4.1.1** using mixtures of xylene and tetrachloroethylene instead of a solution in sucrose. Note the readings of the two hydrometers and apply correction for departure of surface tension from 75 mN/m as follows:

$$C = \frac{\pi\rho D}{g_n m} (\sigma - 75) \times 10^{-3}$$

Where,

C = correction in terms of relative density (20°/4°C) (this has to be converted to degree Brix before adding to each observed reading),

P = relative density (20/4°C) equivalent to the observed readings in degree Brix of the hydrometers,

D = diameter in mm of the stem of the hydrometers,

σ = surface tension of the liquid mixture in mN/m,

g_n = acceleration due to gravity in m/s^2 (9.791 387/ m/s^2 taken as the standard acceleration due to gravity), and

m = mass in g of the hydrometers.

NOTE — The International value of acceleration due to gravity, g , is 9.806 65 m/s^2 .

A-4.1.2.1 Any difference in the corrected readings of the Brix hydrometer under test from that of the standardized hydrometer shall be treated as error at that point. Repeat the test to cover at least four points on the scale.

A-4.2 Pyknometer Method — Weigh a clean dry pyknometer and fill it to a level slightly above the mark on the neck with a solution of sucrose containing a known quantity at 20°C taking care to see that no air gets entrapped in it. Place the pyknometer in the bath for half an hour such that it is immersed in it to a level slightly below the mark. When the pyknometer and its contents have attained the bath temperature, adjust the liquid level such that the meniscus just touches the mark on the neck of the pyknometer. Remove the pyknometer from the bath, wipe with a dry cloth, dry and weigh to determine the mass of the liquid.

A-4.2.1 The true mass of the liquid is calculated by adding to the observed mass of the liquid a correction for the buoyancy effect of the air. This correction is calculated from the following formula:

$$C = p (V - m/d)$$

Where,

C = correction factor,

P = density of air at the temperature of experiment,

V = volume in ml of the liquid in the pyknometer at 20°C,

m = observed mass in g of the liquid, and

d = density of the weights at the temperature of experiment.

A-4.2.2 Calculate the relative density (20/4°C) of the liquid by dividing the mass of the liquid obtained as above, by the volume at 20°C and subsequently find out the equivalent value in degrees Brix from Table 6. Any departure from this value in the reading of the Brix hydrometer tables for the same solution at 20°C separately shall be taken as error at corresponding point on the scale.

ANNEX B
(*Clause 11.1*)
METHOD OF USING BRIX HYDROMETERS

B-1 GENERAL

B-1.1 The determination of percentage of sucrose by mass in sucrose solution with a Brix hydrometer involves:

- a) reading the hydrometer in the liquid at known temperature; and
- b) applying to the observed reading corrections, as necessary, for:
 - i) scale error of the hydrometer (*see A-4.1.1.1, A-4.1.2.1 and A-4.2.2*);
 - ii) correction due to the departure of coefficient of cubical expansion of glass of hydrometer from $25 \times 10^{-6}^{\circ}\text{C}$ (*see Table 4*); and
 - iii) the difference between the temperature of observation and the standard temperature of calibration of hydrometer (*see Table 5*).

B-2 READING OF HYDROMETERS

B-2.1 A convenient method for observing the hydrometer reading in a transparent liquid is to observe the same in a rectangular jar.

B-2.2 The hydrometer and the jar should be clean and dry.

B-3 PROCEDURE

B-3.1 Pour the liquid, whose concentration is to be measured, slowly along the sides of the jar so as not to entrap any air bubble. Allow the liquid in the jar to stand for some time so as to acquire the ambient temperature. If necessary the liquid may be stirred in such a way that no air bubble is formed.

B-3.2 Hold the hydrometer near the tip of the stem and insert it slowly in the liquid till it reaches near the point of balance and then release. The hydrometer will come to rest after a few up and down motions. If the hydrometer has not dripped beyond the point of rest, press the top of the stem slightly so that the hydrometer dips in the liquid a few millimetres beyond the point of test.

B-3.3 Watch the hydrometer when it moves up and down in the liquid. If the stem or the liquid surface is unclean the liquid meniscus formed with the stem will be distorted or dragged with the movement of the hydrometer, otherwise it will remain unchanged with the movement of the hydrometer.

B-3.4 Observe the temperature of the liquid and read the scale at the intersection of liquid surface with the stem of the hydrometer. Note the temperature of the liquid again to ensure that no significant change in temperature of the liquid has taken place during the observation period.

NOTE 1 — The hydrometer should not touch the sides of the vessel when the reading is taken. In reading the hydrometer scale the eye is placed slightly below the plane of the surface of the liquid. It is raised slo

wly until the surface, seen as an ellipse, becomes a straight line. The point where this line cuts the hydrometer scale should be taken as the reading of the hydrometer.

NOTE 2 — In case of viscous liquids allow the hydrometer to settle down to the final position giving adequate time for this purpose.

B-4 APPLICATION OF CORRECTIONS FOR FINAL READING

B-4.1 General

Corrections are applied to the observed reading of a Brix hydrometer, wherever necessary, as follows.

B-4.2 Corrections for Scale Error

In Case there is any difference between the readings of the hydrometer in use and the readings under the same conditions of a similar hydrometer which is known to be standardized (*see A-4.1.1.1, A-4.1.2.1 and A-4.2.2*), the difference so obtained shall be applied for all conditions of use.

B-4.3 Correction for Departure from the Conventional Value of the Coefficient of Cubical Thermal Expansion of Glass of Hydrometer

In case of a departure from the conventional value of the coefficient of cubical thermal expansion of glass used in the manufacture of Brix hydrometer, from 0.000025°C , application to be observed reading of a correction determined as follows, becomes necessary:

$$C = \rho (0.000025 - \gamma) (t - t_3)$$

Where,

C = correction in terms of relative density $20/4^{\circ}\text{C}$ (this is to be converted to degree Brix before adding to the observed reading at $t^{\circ}\text{C}$);

ρ

= relative density $20/4^{\circ}\text{C}$ equivalent to the observed reading in degree Brix of the hydrometer;

γ = coefficient of cubical thermal expansion per degree Celsius of glass of the hydrometer:

t = temperature of observation in degree Celsius; and

t_3 = standard temperature of calibration, that is, 20°C .

Example:

Let the reading of hydrometer be 15° Brix.

The corresponding relative density $20/4^{\circ}\text{C}$ (see Table 6) is 1.05916.

Let the coefficient of thermal cubical expansion of glass of the hydrometer be 0.000010°C and t_1 the temperature of observation be 30°C .

Then $C = 1.05916 (0.000025 - 0.000010) (30 - 20)$

$$= 1.05916 \times 0.000015 \times 10$$

$$= 0.00016 \text{ relative density } 20/4^{\circ}\text{C.}$$

Now from Table 6 it can be seen that near 15°Brix for a difference of 0.1° Brix the difference in relative density is 0.00043. Therefore, 0.000 16 relative density corresponds to 0.037°Brix. Hence, the correction to be added is 0.037°Brix.

B-4.3.1 For the purpose of Brix hydrometers, Table 4 gives this correction. This has been calculated, assuming the value of $(t - t_2) = 1$, in the above equation. Therefore, the value has to be multiplied by the actual value of $(t - t_2)$ before adding to the observed reading. The sign (+) or (-) of the correction will accordingly depend on value of $(t - t_2)$.

Table 4 Correction Applicable To The Reading Of Brix Hydrometers On Account Of Departure From The Standard Coefficient Of Cubical Thermal Expansion Of Glass
(Clauses 8.2.1.1, B-1.1 and B-4.3.1)

| READING OF BRIX HYDROMETER | | VALUE OF $0.000025 - \gamma$ | |
|-------------------------------|--------|------------------------------|--------|
| (1) | (2) | (3) | (4) |
| °Brix | °Brix | °Brix | °Brix |
| 0 to 10 | 0.0026 | 0.0038 | 0.0051 |
| 10 to 20 | 0.0025 | 0.0037 | 0.0050 |
| 20 to 30 | 0.0024 | 0.0036 | 0.0048 |
| 30 to 40 | 0.0023 | 0.0035 | 0.0046 |
| 40 to 50 | 0.0023 | 0.0034 | 0.0045 |
| 50 to 60 | 0.0022 | 0.0033 | 0.0044 |
| 60 to 70 | 0.0022 | 0.0032 | 0.0043 |
| 70 to 80 | 0.0021 | 0.0032 | 0.0043 |
| 80 to 90 | 0.0021 | 0.0032 | 0.0042 |
| 90 to 100 | 0.0021 | 0.0032 | 0.0042 |

γ = coefficient of cubical thermal expansion of glass of Brix hydrometer.

B-4.4 Correction for Difference of Temperature

In case a Brix hydrometer is used at a temperature other than the temperature of its calibration (20° C), correction for difference of temperature has also to be applied as given in Table 5.

B-4.5 The reading corrected by applying necessary corrections (*see B-4.2, B-4.3 and B-4.4*) gives the final reading for the determination of sucrose content, percent by mass, in a solution at 20°C.

Table 5 Corrections for Differences of Temperature (Standard at 20°C)
 (Clause B-4.4)

| OBS ERV ATI ONS TEM PER ATU RE | OBSERVED PERCENTAGE OF SUGAR | | | | | | | | | | | | | |
|---|-----------------------------------|------|------|------|------|------|------|------|------|------|------|------|------|------|
| | 0 | 5 | 10 | 15 | 20 | 25 | 30 | 35 | 40 | 45 | 50 | 55 | 60 | 70 |
| °C | Subtract from Observed Percentage | | | | | | | | | | | | | |
| 0 | 030 | 049 | 065 | 0.77 | 0.89 | 099 | 108 | 116 | 124 | 131 | 137 | 141 | 144 | 1-49 |
| 5 | 036 | 0*47 | 056 | 062 | 073 | 080 | 086 | 091 | 097 | 101 | 1.05 | 108 | 110 | 114 |
| 10 | 032 | 0'38 | 043 | 048 | 052 | 057 | 060 | 064 | 067 | 070 | 072 | 074 | 075 | 077 |
| 11 | 031 | 035 | 040 | 044 | 04S | 051 | 055 | 058 | 060 | 063 | 065 | 066 | 068 | 0'70 |
| 12 | 029 | 0-32 | 036 | 040 | 043 | 046 | 050 | 052 | 054 | 056 | 0-58 | 059 | 060 | 062 |
| 13 | 026 | 029 | 032 | 035 | 038 | 041 | 044 | 046 | 048 | 049 | 051 | 052 | 053 | 055 |
| 14 | 024 | 026 | 029 | 031 | 034 | 036 | 038 | 040 | 041 | 042 | 044 | 045 | 046 | 047 |
| 15 | 020 | 022 | 024 | 026 | 028 | 030 | 032 | 033 | 034 | 036 | 036 | 0-37 | 038 | 0*39 |
| 16 | 017 | 018 | 020 | 022 | 023 | 025 | 026 | 027 | 0*28 | 028 | 029 | 030 | 031 | 032 |
| 17 | 013 | 014 | 015 | 016 | 018 | 019 | 020 | 020 | 021 | 021 | 0'22 | 023 | 023 | 0*24 |
| 17.5 | 011 | 012 | 012 | 014 | 0-15 | 0'16 | 016 | 017 | 017 | 018 | 018 | 019 | 019 | 020 |
| 18 | 009 | 010 | 010 | 011 | 012 | 013 | 013 | 0-14 | 014 | 014 | 015 | 015 | 015 | 016 |
| 19 | 005 | 005 | 0-05 | 006 | 006 | 0-06 | 007 | 007 | 0'07 | 007 | 0-08 | 008 | 008 | 008 |
| | Add to Observed Percentage | | | | | | | | | | | | | |
| 21 | 0.04 | 0.05 | 0.06 | 0.06 | 0.06 | 0.07 | 0.07 | 0.07 | 0.07 | 0.08 | 0.08 | 0.08 | 0.08 | 009 |
| 22 | 0.10 | 0.10 | 0.11 | 0.12 | 0.12 | 0.13 | 0.14 | 0.14 | 0.15 | 0.15 | 0.16 | 0.16 | 0.16 | 016 |
| 23 | 0.16 | 0.16 | 0.17 | 0.17 | 0.19 | 0.20 | 0.21 | 0.21 | 0.22 | 0.23 | 0.24 | .24 | 0.24 | 024 |
| 24 | 0.21 | 0.22 | 0.23 | 0.24 | 0.26 | 0.27 | 0.28 | 0.29 | 0.30 | 0.31 | 0.32 | 032 | 0.32 | 032 |
| 25 | 0.27 | 0.28 | 0.30 | 0.31 | 0.32 | 0.34 | 0.35 | 0.36 | 0.38 | 0.38 | 0.39 | 0.39 | 0.40 | 0.39 |
| 26 | 0.33 | 0.34 | 0.36 | 0.37 | 0.40 | 0.40 | 0.42 | 0.44 | 0.46 | 0.47 | 0.47 | 0.48 | 0.48 | 0.48 |
| 27 | 0.40 | 0.41 | 0.42 | 0.44 | 0.45 | 0.48 | 0.50 | 052 | 054 | 0.54 | 0.55 | 0.56 | 0.56 | 056 |
| 28 | 0.46 | 0.47 | 0.49 | 0.51 | 0.54 | 0.56 | 0.58 | 0.60 | 0.61 | 0.62 | 0.63 | 0.64 | 0.64 | 0.64 |
| 29 | 0.54 | 0.55 | 056 | 0.59 | 0.61 | 0.63 | 0.66 | 0.68 | 0.70 | 0.70 | 0.71 | 0.72 | 0.72 | 0.72 |
| 30 | 0.61 | 0.62 | 0.63 | 0.66 | 0.68 | 0.71 | 0.73 | 0.76 | 0.78 | 0.73 | 0.79 | 0.80 | 0.80 | 0.81 |
| 35 | 0.99 | 1.01 | 1.02 | 1.06 | 1.10 | 1.13 | 1.16 | 1.18 | 1.20 | 1.21 | 1.22 | 1.22 | 1.23 | 1.22 |
| 40 | 1.42 | 1.45 | 1.47 | 1.51 | 1.54 | 1.57 | 1.60 | 1.62 | 1.64 | 1.65 | 1.65 | 1.65 | 1.66 | 1.65 |
| 45 | 1.91 | 1.94 | 1.96 | 2.00 | 2.03 | 2.05 | 207 | 2.09 | 2.10 | 2.10 | 2.10 | 2.10 | 2.10 | 2.08 |
| 50 | 2.46 | 2.48 | 2.50 | 2.53 | 2.56 | 2.57 | 2.58 | 2.59 | 2.59 | 2.58 | 2.58 | 2.57 | 2.56 | 2.52 |

| | | | | | | | | | | | | | | |
|----|------|------|------|------|------|------|------|------|------|------|------|------|------|------|
| 55 | 3.05 | 3.07 | 3.09 | 3.12 | 3.12 | 3.12 | 3.12 | 3.11 | 3.10 | 3.08 | 3.07 | 3.05 | 3.03 | 2.97 |
| 60 | 3.69 | 3.72 | 3.73 | 3.73 | 3.72 | 3.70 | 3.67 | 3.65 | 3.62 | 3.60 | 3.57 | 3.54 | 3.50 | 3.43 |
| 65 | 4.4 | 4.4 | 4.4 | 4.4 | 4.4 | 4.4 | 4.3 | 4.2 | 4.2 | 4.1 | 4.1 | 4.0 | 4.0 | 3.9 |
| 70 | 5.1 | 5.1 | 5.1 | 5.0 | 5.0 | 5.0 | 4.9 | 4.8 | 4.8 | 4.7 | 4.7 | 4.6 | 4.6 | 4.4 |
| 75 | 6.1 | 6.0 | 6.0 | 5.9 | 5.8 | 5.8 | 5.7 | 5.6 | 5.5 | 5.4 | 5.4 | 5.3 | 5.2 | 5.0 |
| 80 | 7.1 | 7.0 | 7.0 | 6.9 | 6.8 | 6.7 | 6.6 | 6.4 | 6.3 | 6.2 | 6.1 | 6.0 | 5.9 | 5.9 |

Table 6 Degrees Brix and Relative Density of Sugar Solution
(*Clauses A-4.2.2 and B-4.2*)

| DEGREES BRX OR PERCENT AGE OF SUCROSE BY WEIGHT (1) | RELATI VE DENSIT Y AT 20/4°C (2) | DEGREES BRX OR PERCENT AGE OF SUCROSE BY WEIGHT (1) | RELATI VE DENSIT Y AT 20/4°C (2) | DEGREES BRX OR PERCENT AGE OF SUCROSE BY WEIGHT (1) | RELATI VE DENSIT Y AT 20/4°C (2) | DEGREES BRX OR PERCENT AGE OF SUCROSE BY WEIGHT (1) | RELATI VE DENSIT Y AT 20/4°C (2) |
|--|---|--|---|--|---|--|---|
| 0.0 | 0.99823 | 25.1 | 1.10402 | 50.1 | 1.23012 | 75.1 | 1.37962 |
| 0.1 | 0.99862 | 25.2 | 1.10448 | 50.2 | 1.23067 | 75.2 | 1.38026 |
| 0.2 | 0.99901 | 25.3 | 1.10494 | 50.3 | 1.23122 | 75.3 | 1.38091 |
| 0.3 | 0.99940 | 25.4 | 1.10540 | 50.4 | 1.23177 | 75.4 | 1.38156 |
| 0.4 | 0.99979 | 25.5 | 1.10586 | 50.5 | 1.23232 | 75.5 | 1.38220 |
| 0.5 | 1.00017 | 25.6 | 1.10632 | 50.6 | 1.23287 | 75.6 | 1.38285 |
| 0.6 | 1.00056 | 25.7 | 1.10679 | 50.7 | 1.23343 | 75.7 | 1.38350 |
| 0.7 | 1.00095 | 25.8 | 1.10725 | 50.8 | 1.23398 | 75.8 | 1.38415 |
| 0.8 | 1.00134 | 25.9 | 1.10771 | 50.9 | 1.23453 | 75.9 | 1.38480 |
| 0.9 | 1.00173 | 26.0 | 1.10818 | 51.0 | 1.23508 | 76.0 | 1.38545 |
| 1.0 | 1.00212 | 26.1 | 1.10864 | 51.1 | 1.23564 | 76.1 | 1.38610 |
| 1.1 | 1.00251 | 26.2 | 1.10957 | 51.2 | 1.23619 | 76.2 | 1.38675 |
| 1.2 | 1.00290 | 26.3 | 1.10957 | 51.3 | 1.23675 | 76.3 | 1.38740 |
| 1.3 | 1.00329 | 26.4 | 1.11003 | 51.4 | 1.23730 | 76.4 | 1.38805 |
| 1.4 | 1.00368 | 26.5 | 1.11050 | 51.5 | 1.23786 | 76.5 | 1.38875 |
| 1.5 | 1.00406 | 26.6 | 1.11096 | 51.6 | 1.23841 | 76.6 | 1.38835 |
| 1.6 | 1.00445 | 26.7 | 1.11143 | 51.7 | 1.23897 | 76.7 | 1.39000 |
| 1.7 | 1.00484 | 26.8 | 1.11190 | 51.8 | 1.23953 | 76.8 | 1.39065 |
| 1.8 | 1.00523 | 26.9 | 1.11236 | 51.9 | 1.24008 | 76.9 | 1.39130 |
| 1.9 | 1.00562 | 27.0 | 1.11283 | 52.0 | 1.24064 | 77.0 | 1.39196 |
| 2.0 | 1.00602 | 27.1 | 1.11330 | 52.1 | 1.24120 | 77.1 | 1.39261 |
| 2.1 | 1.00641 | 27.2 | 1.11376 | 52.2 | 1.24176 | 77.2 | 1.39326 |
| 2.2 | 1.00680 | 27.3 | 1.11423 | 52.3 | 1.24232 | 77.3 | 1.39392 |
| 2.3 | 1.00719 | 27.4 | 1.11470 | 52.4 | 1.24287 | 77.4 | 1.39457 |
| 2.4 | 1.00758 | 27.5 | 1.11517 | 52.5 | 1.24343 | 77.5 | 1.39523 |
| 2.5 | 1.00797 | 27.6 | 1.11564 | 52.6 | 1.24399 | 77.6 | 1.39588 |
| 2.6 | 1.00836 | 27.7 | 1.11610 | 52.7 | 1.24455 | 77.7 | 1.39654 |
| 2.7 | 1.00876 | 27.8 | 1.11657 | 52.8 | 1.24511 | 77.8 | 1.39719 |
| 2.8 | 1.00915 | 27.9 | 1.11704 | 52.9 | 1.24567 | 77.9 | 1.39785 |

| | | | | | | | |
|-----|---------|------|---------|------|---------|------|---------|
| 2.9 | 1.00954 | 28.0 | 1.11751 | 53.0 | 1.24623 | 78.0 | 1.39850 |
| 3.0 | 1.00993 | 28.1 | 1.11798 | 53.1 | 1.24680 | 78.1 | 1.39916 |
| 3.1 | 1.01033 | 28.2 | 1.11845 | 53.2 | 1.24736 | 78.2 | 1.39982 |
| 3.2 | 1.01072 | 28.3 | 1.11892 | 53.3 | 1.24792 | 78.3 | 1.40048 |
| 3.3 | 1.01112 | 28.4 | 1.11940 | 53.4 | 1.24848 | 78.4 | 1.40113 |
| 3.4 | 1.01151 | 28.5 | 1.11987 | 53.5 | 1.24905 | 78.5 | 1.40179 |
| 3.5 | 1.01190 | 28.6 | 1.12034 | 53.6 | 1.24961 | 78.6 | 1.40245 |
| 3.6 | 1.01230 | 28.7 | 1.12081 | 53.7 | 1.25017 | 78.7 | 1.40311 |
| 3.7 | 1.01269 | 28.8 | 1.12128 | 53.8 | 1.25074 | 78.8 | 1.40377 |
| 3.8 | 1.01309 | 28.9 | 1.12176 | 53.9 | 1.25130 | 78.9 | 1.40443 |
| 3.9 | 1.01348 | 29.0 | 1.12223 | 54.0 | 1.25187 | 79.0 | 1.40509 |
| 4.0 | 1.01388 | 29.1 | 1.12270 | 54.1 | 1.25243 | 79.1 | 1.40575 |
| 4.1 | 1.01428 | 29.2 | 1.12318 | 54.2 | 1.25300 | 79.2 | 1.40641 |
| 4.2 | 1.01467 | 29.3 | 1.12365 | 54.3 | 1.25356 | 79.3 | 1.40707 |
| 4.3 | 1.01507 | 29.4 | 1.12413 | 54.4 | 1.25413 | 79.4 | 1.40774 |
| 4.4 | 1.01547 | 29.5 | 1.12460 | 54.5 | 1.25470 | 79.5 | 1.40840 |
| 4.5 | 1.01586 | 29.6 | 1.12508 | 54.6 | 1.25526 | 79.6 | 1.40906 |
| 4.6 | 1.01626 | 29.7 | 1.12556 | 54.7 | 1.25583 | 79.7 | 1.40972 |
| 4.7 | 1.01666 | 29.8 | 1.12603 | 54.8 | 1.25640 | 79.8 | 1.41039 |
| 4.8 | 1.01706 | 29.9 | 1.12651 | 54.9 | 1.25697 | 79.9 | 1.41105 |
| 4.9 | 1.01746 | 30.0 | 1.12698 | 55.0 | 1.25754 | 80.0 | 1.41172 |
| 5.0 | 1.01785 | 30.1 | 1.12746 | 55.1 | 1.25810 | 80.1 | 1.41238 |
| 5.1 | 1.01825 | 30.2 | 1.12794 | 55.2 | 1.25867 | 80.2 | 1.41304 |
| 5.2 | 1.01865 | 30.3 | 1.12842 | 55.3 | 1.25924 | 80.3 | 1.41371 |
| 5.3 | 1.01905 | 30.4 | 1.12890 | 55.4 | 1.25982 | 80.4 | 1.41437 |
| 5.4 | 1.01945 | 30.5 | 1.12937 | 55.5 | 1.26039 | 80.5 | 1.41504 |
| 5.5 | 1.01985 | 30.6 | 1.12985 | 55.6 | 1.26096 | 80.6 | 1.41571 |
| 5.6 | 1.02025 | 30.7 | 1.13033 | 55.7 | 1.26153 | 80.7 | 1.41637 |
| 5.7 | 1.02065 | 30.8 | 1.13081 | 55.8 | 1.26210 | 80.8 | 1.41704 |
| 5.8 | 1.02105 | 30.9 | 1.13129 | 55.9 | 1.26267 | 80.9 | 1.41771 |
| 5.9 | 1.02145 | 31.0 | 1.13177 | 56.0 | 1.26324 | 81.0 | 1.41837 |
| 6.0 | 1.02186 | 31.1 | 1.13225 | 56.1 | 1.26382 | 81.1 | 1.41904 |
| 6.1 | 1.02226 | 31.2 | 1.13274 | 56.2 | 1.26439 | 81.2 | 1.41971 |
| 6.2 | 1.02266 | 31.3 | 1.13322 | 56.3 | 1.26496 | 81.3 | 1.42038 |
| 6.3 | 1.02306 | 31.4 | 1.13370 | 56.4 | 1.26554 | 81.4 | 1.42105 |
| 6.4 | 1.02346 | 31.5 | 1.13418 | 56.5 | 1.26611 | 81.5 | 1.42172 |
| 6.5 | 1.02387 | 31.6 | 1.13466 | 56.6 | 1.26669 | 81.6 | 1.42239 |
| 6.6 | 1.02427 | 31.7 | 1.13515 | 56.7 | 1.26726 | 81.7 | 1.42306 |
| 6.7 | 1.02467 | 31.8 | 1.13563 | 56.8 | 1.26784 | 81.8 | 1.42373 |
| 6.8 | 1.02508 | 31.9 | 1.13611 | 56.9 | 1.26841 | 81.9 | 1.42440 |
| 6.9 | 1.02548 | 32.0 | 1.13660 | 57.0 | 1.26899 | 82.0 | 1.42507 |
| 7.0 | 1.02588 | 32.1 | 1.13708 | 57.1 | 1.26956 | 82.1 | 1.42574 |
| 7.1 | 1.02629 | 32.2 | 1.13756 | 57.2 | 1.27014 | 82.2 | 1.42642 |
| 7.2 | 1.02669 | 32.3 | 1.13805 | 57.3 | 1.27072 | 82.3 | 1.42709 |
| 7.3 | 1.02710 | 32.4 | 1.13853 | 57.4 | 1.27130 | 82.4 | 1.42776 |
| 7.4 | 1.02750 | 32.5 | 1.13902 | 57.5 | 1.27188 | 82.5 | 1.42844 |
| 7.5 | 1.02791 | 32.6 | 1.13951 | 57.6 | 1.27246 | 82.6 | 1.42911 |
| 7.6 | 1.02832 | 32.7 | 1.13999 | 57.7 | 1.27304 | 82.7 | 1.42978 |
| 7.7 | 1.02872 | 32.8 | 1.14048 | 57.8 | 1.27361 | 82.8 | 1.43046 |
| 7.8 | 1.02913 | 32.9 | 1.14097 | 57.9 | 1.27419 | 82.9 | 1.43113 |

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|------|---------|------|---------|------|---------|------|---------|
| 7.9 | 1.02954 | 33.0 | 1.14143 | 58.0 | 1.27477 | 83.0 | 1.43181 |
| 8.0 | 1.02994 | 33.1 | 1.14194 | 58.1 | 1.27535 | 83.1 | 1.43248 |
| 8.1 | 1.03035 | 33.2 | 1.14243 | 58.2 | 1.27594 | 83.2 | 1.43316 |
| 8.2 | 1.03076 | 33.3 | 1.14292 | 58.3 | 1.27652 | 83.3 | 1.43384 |
| 8.3 | 1.03116 | 33.4 | 1.14340 | 58.4 | 1.27710 | 83.4 | 1.43451 |
| 8.4 | 1.03157 | 33.5 | 1.14389 | 58.5 | 1.27768 | 83.5 | 1.43519 |
| 8.5 | 1.03198 | 33.6 | 1.14438 | 58.6 | 1.27826 | 83.6 | 1.43587 |
| 8.6 | 1.03280 | 33.7 | 1.14487 | 58.7 | 1.27884 | 83.7 | 1.43654 |
| 8.7 | 1.03321 | 33.8 | 1.14536 | 58.8 | 1.279 | 83.8 | 1.43722 |
| 8.8 | 1.03362 | 33.9 | 1.14585 | 58.9 | 1.2801 | 83.9 | 1.43790 |
| 8.9 | 1.03403 | 34.0 | 1.14634 | 59.0 | 1.28060 | 84.0 | 1.43858 |
| 9.0 | 1.03444 | 34.1 | 1.14584 | 59.1 | 1.28118 | 84.1 | 1.43926 |
| 9.1 | 1.03485 | 34.2 | 1.14733 | 59.2 | 1.28176 | 84.2 | 1.43994 |
| 9.2 | 1.03526 | 34.3 | 1.14782 | 59.3 | 1.28235 | 84.3 | 1.44062 |
| 9.3 | 1.03567 | 34.4 | 1.14831 | 59.4 | 1.28252 | 84.4 | 1.44130 |
| 9.4 | 1.03608 | 34.5 | 1.14880 | 59.5 | 1.28411 | 84.5 | 1.44198 |
| 9.5 | 1.03649 | 34.6 | 1.14930 | 59.6 | 1.28469 | 84.6 | 1.44266 |
| 9.6 | 1.03691 | 34.7 | 1.14979 | 59.7 | 1.28528 | 84.7 | 1.44334 |
| 9.7 | 1.03732 | 34.8 | 1.15029 | 59.8 | 1.28587 | 84.8 | 1.44402 |
| 9.8 | 1.03773 | 34.9 | 1.15078 | 59.9 | 1.28587 | 84.9 | 1.44470 |
| 9.9 | 1.03814 | 35.0 | 1.15128 | 60.0 | 1.28646 | 85.0 | 1.44539 |
| 10.0 | 1.03856 | 35.1 | 1.15177 | 60.1 | 1.28704 | 85.1 | 1.44607 |
| 10.1 | 1.03897 | 35.2 | 1.15226 | 60.2 | 1.28763 | 85.2 | 1.44675 |
| 10.2 | 1.03938 | 35.3 | 1.15276 | 60.3 | 1.28822 | 85.3 | 1.44744 |
| 10.3 | 1.03980 | 35.4 | 1.15326 | 60.4 | 1.28881 | 85.4 | 1.44812 |
| 10.4 | 1.04021 | 35.5 | 1.15375 | 60.5 | 1.28940 | 85.5 | 1.44881 |
| 10.5 | 1.04063 | 35.6 | 1.15425 | 60.6 | 1.28999 | 85.6 | 1.44949 |
| 10.6 | 1.04104 | 35.7 | 1.15475 | 60.7 | 1.29058 | 85.7 | 1.45018 |
| 10.7 | 1.04146 | 35.8 | 1.15524 | 60.8 | 1.29117 | 85.8 | 1.45086 |
| 10.8 | 1.04187 | 35.9 | 1.15574 | 60.9 | 1.29176 | 85.9 | 1.45154 |
| 10.9 | 1.04229 | 36.0 | 1.15624 | 61.0 | 1.29235 | 86.0 | 1.45223 |
| 11.0 | 1.04270 | 36.1 | 1.15674 | 61.1 | 1.29295 | 86.1 | 1.45292 |
| 11.1 | 1.04312 | 36.2 | 1.15724 | 61.2 | 1.29354 | 86.2 | 1.45360 |
| 11.2 | 1.04354 | 36.3 | 1.15773 | 61.3 | 1.29413 | 86.3 | 1.45429 |
| 11.3 | 1.04395 | 36.4 | 1.15823 | 61.4 | 1.29472 | 86.4 | 1.45498 |
| 11.4 | 1.04437 | 36.5 | 1.15873 | 61.5 | 1.29532 | 86.5 | 1.45567 |
| 11.5 | 1.04479 | 36.6 | 1.15923 | 61.6 | 1.29591 | 86.6 | 1.45636 |
| 11.6 | 1.04521 | 36.7 | 1.15973 | 61.7 | 1.29651 | 86.7 | 1.45704 |
| 11.7 | 1.04521 | 36.8 | 1.16023 | 61.8 | 1.29710 | 86.8 | 1.45773 |
| 11.8 | 1.04562 | 36.9 | 1.16073 | 61.9 | 1.2977 | 86.9 | 1.45842 |
| 11.9 | 1.04604 | 37.0 | 1.16124 | 62.0 | 1.29829 | 87.0 | 1.45911 |
| 12.0 | 1.04646 | 37.1 | 1.16174 | 62.1 | 1.29889 | 87.1 | 1.45980 |
| 12.1 | 1.04688 | 37.2 | 1.16224 | 62.2 | 1.29948 | 87.2 | 1.46052 |
| 12.2 | 1.04730 | 37.3 | 1.16274 | 62.3 | 1.30008 | 87.3 | 1.46119 |
| 12.3 | 1.04772 | 37.4 | 1.16324 | 62.4 | 1.30068 | 87.4 | 1.46188 |
| 12.4 | 1.04814 | 37.5 | 1.16375 | 62.5 | 1.30127 | 87.5 | 1.46257 |
| 12.5 | 1.04856 | 37.6 | 1.16425 | 62.6 | 1.30187 | 87.6 | 1.46326 |
| 12.6 | 1.04898 | 37.7 | 1.16476 | 62.7 | 1.30247 | 87.7 | 1.46395 |
| 12.7 | 1.04940 | 37.8 | 1.16526 | 62.8 | 1.30307 | 87.8 | 1.46464 |
| 12.8 | 1.04982 | 37.9 | 1.16576 | 62.9 | 1.30367 | 87.9 | 1.46534 |

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|------|---------|------|---------|------|---------|------|---------|
| 12.9 | 1.05024 | 38.0 | 1.16627 | 63.0 | 1.30427 | 88.0 | 1.46603 |
| 13.0 | 1.05066 | 38.1 | 1.16678 | 63.1 | 1.30487 | 88.1 | 1.46673 |
| 13.1 | 1.05109 | 38.2 | 1.16728 | 63.2 | 1.30587 | 88.2 | 1.46742 |
| 13.2 | 1.05151 | 38.3 | 1.16779 | 63.3 | 1.30607 | 88.3 | 1.46812 |
| 13.3 | 1.05193 | 38.4 | 1.16829 | 63.4 | 1.30667 | 88.4 | 1.46881 |
| 13.4 | 1.05236 | 38.5 | 1.16880 | 63.5 | 1.30727 | 88.5 | 1.46950 |
| 13.5 | 1.05278 | 38.6 | 1.16931 | 63.6 | 1.30787 | 88.6 | 1.47020 |
| 13.6 | 1.05320 | 38.7 | 1.16982 | 63.7 | 1.30848 | 88.7 | 1.47090 |
| 13.7 | 1.05363 | 38.8 | 1.17032 | 63.8 | 1.30908 | 88.8 | 1.47159 |
| 13.8 | 1.05406 | 38.9 | 1.17083 | 63.9 | 1.30968 | 88.9 | 1.47229 |
| 13.9 | 1.05448 | 39.0 | 1.17134 | 64.0 | 1.31028 | 89.0 | 1.47299 |
| 14.0 | 1.05490 | 39.1 | 1.17185 | 64.1 | 1.31088 | 89.1 | 1.47368 |
| 14.1 | 1.05531 | 39.2 | 1.17236 | 64.2 | 1.31149 | 89.2 | 1.47238 |
| 14.2 | 1.05575 | 39.3 | 1.17287 | 64.3 | 1.31209 | 89.3 | 1.47508 |
| 14.3 | 1.05618 | 39.4 | 1.17338 | 64.4 | 1.31270 | 89.4 | 1.47278 |
| 14.4 | 1.05660 | 39.5 | 1.17389 | 64.5 | 1.31330 | 89.5 | 1.47648 |
| 14.5 | 1.05703 | 39.6 | 1.17440 | 64.6 | 1.31391 | 89.6 | 1.47718 |
| 14.6 | 1.05746 | 39.7 | 1.17491 | 64.7 | 1.31452 | 89.7 | 1.17788 |
| 14.7 | 1.05788 | 39.8 | 1.17542 | 64.8 | 1.31512 | 89.8 | 1.47858 |
| 14.8 | 1.05831 | 39.9 | 1.17594 | 64.9 | 1.31573 | 89.9 | 1.47928 |
| 14.9 | 1.05874 | 40.0 | 1.17645 | 65.0 | 1.31633 | 90.0 | 1.47998 |
| 15.0 | 1.05916 | 40.1 | 1.17696 | 65.1 | 1.31694 | 90.1 | 1.48068 |
| 15.1 | 1.05959 | 40.2 | 1.17747 | 65.2 | 1.31755 | 90.2 | 1.48136 |
| 15.2 | 1.06002 | 40.3 | 1.17799 | 65.3 | 1.31816 | 90.3 | 1.48208 |
| 15.3 | 1.06045 | 40.4 | 1.17850 | 65.4 | 1.31877 | 90.4 | 1.48278 |
| 15.4 | 1.06088 | 40.5 | 1.17901 | 65.5 | 1.31937 | 90.5 | 1.48348 |
| 15.5 | 1.06131 | 40.6 | 1.17953 | 65.6 | 1.31998 | 90.6 | 1.48419 |
| 15.6 | 1.06174 | 40.7 | 1.18004 | 65.7 | 1.32059 | 90.7 | 1.48489 |
| 15.7 | 1.06217 | 40.8 | 1.18056 | 65.8 | 1.32120 | 90.8 | 1.48559 |
| 15.8 | 1.06260 | 40.9 | 1.18108 | 65.9 | 1.32181 | 90.9 | 1.48630 |
| 15.9 | 1.06303 | 41.0 | 1.18159 | 66.0 | 1.32242 | 91.0 | 1.48700 |
| 16.0 | 1.06346 | 41.1 | 1.18211 | 66.1 | 1.32204 | 91.1 | 1.48771 |
| 16.1 | 1.06389 | 41.2 | 1.18262 | 66.2 | 1.32365 | 91.2 | 1.48841 |
| 16.2 | 1.06432 | 41.3 | 1.18314 | 66.3 | 1.32426 | 91.3 | 1.48912 |
| 16.3 | 1.06476 | 41.4 | 1.18366 | 66.4 | 1.32487 | 91.4 | 1.48982 |
| 16.4 | 1.06519 | 41.5 | 1.18418 | 66.5 | 1.32548 | 91.5 | 1.49053 |
| 16.5 | 1.06562 | 41.6 | 1.18470 | 66.6 | 1.32610 | 91.6 | 1.49123 |
| 16.6 | 1.06605 | 41.7 | 1.18522 | 66.7 | 1.32671 | 91.7 | 1.49194 |
| 16.7 | 1.06649 | 41.8 | 1.18573 | 66.8 | 1.32732 | 91.8 | 1.49265 |
| 16.8 | 1.06692 | 41.9 | 1.18625 | 66.9 | 1.32794 | 91.9 | 1.49336 |
| 16.9 | 1.06736 | 42.0 | 1.18677 | 67.0 | 1.32855 | 92.0 | 1.49406 |
| 17.0 | 1.06779 | 42.1 | 1.18729 | 67.1 | 1.32917 | 92.1 | 1.49477 |
| 17.1 | 1.06822 | 42.2 | 1.18781 | 67.2 | 1.32978 | 92.2 | 1.49548 |
| 17.2 | 1.06866 | 42.3 | 1.18834 | 67.3 | 1.33040 | 92.3 | 1.49619 |
| 17.3 | 1.06909 | 42.4 | 1.18886 | 67.4 | 1.33102 | 92.4 | 1.49690 |
| 17.4 | 1.06953 | 42.5 | 1.18938 | 67.5 | 1.33163 | 92.5 | 1.49761 |
| 17.5 | 1.06996 | 42.6 | 1.18990 | 67.6 | 1.33225 | 92.6 | 1.49832 |
| 17.6 | 1.07040 | 42.7 | 1.19042 | 67.7 | 1.33287 | 92.7 | 1.40903 |
| 17.7 | 1.07084 | 42.8 | 1.19095 | 67.8 | 1.33348 | 92.8 | 1.49974 |
| 17.8 | 1.07127 | 42.9 | 1.19147 | 67.9 | 1.33410 | 92.9 | 1.50045 |

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|------|---------|------|---------|------|---------|------|---------|
| 17.9 | 1.07171 | 43.0 | 1.19199 | 68.0 | 1.33472 | 93.0 | 1.50116 |
| 18.0 | 1.07215 | 43.1 | 1.19252 | 68.1 | 1.33534 | 93.1 | 1.50187 |
| 18.1 | 1.07258 | 43.2 | 1.19304 | 68.2 | 1.33596 | 93.2 | 1.50258 |
| 18.2 | 1.07302 | 43.3 | 1.19356 | 68.3 | 1.33658 | 93.3 | 1.50329 |
| 18.3 | 1.07340 | 43.4 | 1.19409 | 68.4 | 1.33720 | 93.4 | 1.50401 |
| 18.4 | 1.07390 | 43.5 | 1.19462 | 68.5 | 1.33782 | 93.5 | 1.50472 |
| 18.5 | 1.07434 | 43.6 | 1.19514 | 68.6 | 1.33844 | 93.6 | 1.50543 |
| 18.6 | 1.07478 | 43.7 | 1.19567 | 68.7 | 1.33906 | 93.7 | 1.50615 |
| 18.7 | 1.07522 | 43.8 | 1.19619 | 68.8 | 1.33968 | 93.8 | 1.50686 |
| 18.8 | 1.07566 | 43.9 | 1.19672 | 68.9 | 1.34031 | 93.9 | 1.50757 |
| 18.9 | 1.07610 | 44.0 | 1.19725 | 69.0 | 1.34093 | 94.0 | 1.50829 |
| 19.0 | 1.07654 | 44.1 | 1.19778 | 69.1 | 1.34155 | 94.1 | 1.50900 |
| 19.1 | 1.07698 | 44.2 | 1.19830 | 69.2 | 1.34217 | 94.2 | 1.50972 |
| 19.2 | 1.07742 | 44.3 | 1.19883 | 69.3 | 1.34280 | 94.3 | 1.51044 |
| 19.3 | 1.07786 | 44.4 | 1.19936 | 69.4 | 1.34342 | 94.4 | 1.51115 |
| 19.4 | 1.07830 | 44.5 | 1.19989 | 69.5 | 1.34405 | 94.5 | 1.51187 |
| 19.5 | 1.07874 | 44.6 | 1.20042 | 69.6 | 1.34467 | 94.6 | 1.51258 |
| 19.6 | 1.07919 | 44.7 | 1.20095 | 69.7 | 1.34530 | 94.7 | 1.51330 |
| 19.7 | 1.07963 | 44.8 | 1.20148 | 69.8 | 1.34530 | 94.8 | 1.51402 |
| 19.8 | 1.08007 | 44.9 | 1.70201 | 69.9 | 1.34655 | 94.9 | 1.51474 |
| 19.9 | 1.08052 | 45.0 | 1.20254 | 70.0 | 1.34717 | 95.0 | 1.51546 |
| 20.0 | 1.08096 | 45.1 | 1.20307 | 70.1 | 1.34780 | 95.1 | 1.51617 |
| 20.1 | 1.08140 | 45.2 | 1.20360 | 70.2 | 1.34843 | 95.2 | 1.51689 |
| 20.2 | 1.08185 | 45.3 | 1.20414 | 70.3 | 1.34906 | 95.3 | 1.51761 |
| 20.3 | 1.08229 | 45.4 | 1.20467 | 70.4 | 1.34968 | 95.4 | 1.51833 |
| 20.4 | 1.08274 | 45.5 | 1.20520 | 70.5 | 1.35031 | 95.5 | 1.51905 |
| 20.5 | 1.08318 | 45.6 | 1.20573 | 70.6 | 1.35094 | 95.6 | 1.51977 |
| 20.6 | 1.08363 | 45.7 | 1.20627 | 70.7 | 1.35157 | 95.7 | 1.52049 |
| 20.7 | 1.08407 | 45.8 | 1.20680 | 70.8 | 1.35220 | 95.8 | 1.52121 |
| 20.8 | 1.08452 | 45.9 | 1.20734 | 70.9 | 1.35283 | 95.9 | 1.52193 |
| 20.9 | 1.08497 | 46.0 | 1.20787 | 71.0 | 1.35346 | 96.0 | 1.52266 |
| 21.0 | 1.08541 | 46.1 | 1.20840 | 71.1 | 1.35409 | 96.1 | 4.52338 |
| 21.1 | 1.08586 | 46.2 | 1.20894 | 71.2 | 1.35472 | 96.2 | 1.52410 |
| 21.2 | 1.08631 | 46.3 | 1.20948 | 71.3 | 1.35535 | 96.3 | 1.52482 |
| 21.3 | 1.08676 | 46.4 | 1.21001 | 71.4 | 1.35598 | 96.4 | 1.52555 |
| 21.4 | 1.08720 | 46.5 | 1.21055 | 71.5 | 1.35661 | 96.5 | 1.52627 |
| 21.5 | 1.08765 | 46.6 | 1.21109 | 71.6 | 1.35724 | 96.6 | 1.52699 |
| 21.6 | 1.08810 | 46.7 | 1.21162 | 71.7 | 1.35788 | 96.7 | 1.52772 |
| 21.7 | 1.08855 | 46.8 | 1.21216 | 71.8 | 1.35851 | 96.8 | 1.52844 |
| 21.8 | 1.08900 | 46.9 | 1.21270 | 71.9 | 1.35914 | 96.9 | 1.52917 |
| 21.9 | 1.08945 | 47.0 | 1.21324 | 72.0 | 1.35978 | 97.0 | 1.52989 |
| 22.0 | 1.08990 | 47.1 | 1.21378 | 72.1 | 1.36041 | 97.1 | 1.53062 |
| 22.1 | 1.09055 | 47.2 | 1.21432 | 72.2 | 1.36105 | 97.2 | 1.53131 |
| 22.2 | 1.09086 | 47.3 | 1.21486 | 72.3 | 1.36168 | 97.3 | 1.53207 |
| 22.3 | 1.09125 | 47.4 | 1.21540 | 72.4 | 1.36232 | 97.4 | 1.53279 |
| 22.4 | 1.09370 | 47.5 | 1.21594 | 72.5 | 1.36295 | 97.5 | 1.53352 |
| 22.5 | 1.09216 | 47.6 | 1.21648 | 72.6 | 1.36359 | 97.6 | 1.53425 |
| 22.6 | 1.09261 | 47.7 | 1.21702 | 72.7 | 1.36423 | 97.7 | 1.53498 |
| 22.7 | 1.09306 | 47.8 | 1.21756 | 72.8 | 1.36486 | 97.8 | 1.53570 |
| 22.8 | 1.09351 | 47.9 | 1.21810 | 72.9 | 1.36550 | 97.9 | 1.53643 |

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|------|---------|------|---------|------|---------|-------|---------|
| 22.9 | 1.09397 | 48.0 | 1.21864 | 73.0 | 1.36614 | 98.0 | 1.53716 |
| 23.0 | 1.09442 | 48.1 | 1.21918 | 73.1 | 1.36678 | 98.1 | 1.53789 |
| 23.1 | 1.09448 | 48.2 | 1.21973 | 73.2 | 1.36742 | 98.2 | 1.53862 |
| 23.2 | 1.09535 | 48.3 | 1.22027 | 73.3 | 1.36805 | 98.3 | 1.53935 |
| 23.3 | 1.09578 | 48.4 | 1.22082 | 73.4 | 1.36869 | 98.4 | 1.54008 |
| 23.4 | 1.09624 | 48.5 | 1.22136 | 73.5 | 1.36933 | 98.5 | 1.54081 |
| 23.5 | 1.09669 | 48.6 | 1.22190 | 73.6 | 1.36997 | 98.6 | 1.54154 |
| 23.6 | 1.09715 | 48.7 | 1.22245 | 73.7 | 1.37061 | 98.7 | 1.54227 |
| 23.7 | 1.09740 | 48.8 | 1.22300 | 73.8 | 1.37125 | 98.8 | 1.54300 |
| 23.8 | 1.09806 | 48.9 | 1.22354 | 73.9 | 1.37189 | 98.9 | 1.54373 |
| 23.9 | 1.09851 | 49.0 | 1.22409 | 74.0 | 1.37254 | 99.0 | 1.54446 |
| 24.0 | 1.09897 | 49.1 | 1.22463 | 74.1 | 1.37318 | 99.1 | 1.54519 |
| 24.1 | 1.09943 | 49.2 | 1.22518 | 74.2 | 1.37382 | 99.2 | 1.54593 |
| 24.2 | 1.09989 | 49.3 | 1.22573 | 74.3 | 1.37446 | 99.3 | 1.54666 |
| 24.3 | 1.10034 | 49.4 | 1.22627 | 74.4 | 1.37510 | 99.4 | 1.54739 |
| 24.4 | 1.10080 | 49.5 | 1.22682 | 74.5 | 1.37575 | 99.5 | 1.54813 |
| 24.5 | 1.10126 | 49.6 | 1.22737 | 74.6 | 1.37639 | 99.6 | 1.54886 |
| 24.6 | 1.10172 | 49.7 | 1.22792 | 74.7 | 1.37704 | 99.7 | 1.54960 |
| 24.7 | 1.10218 | 49.8 | 1.22847 | 74.8 | 1.37768 | 99.8 | 1.55033 |
| 24.8 | 1.10264 | 49.9 | 1.22902 | 74.9 | 1.37833 | 99.9 | 1.55106 |
| 24.9 | 1.10310 | 50.0 | 1.22957 | 75.0 | 1.37897 | 100.0 | 1.55180 |
| 25.0 | 1.10356 | | | | | | |